

constrained systems in general

- Arbitrary number of particles $\alpha = 1 \dots N$ with positions \vec{r}_α
- ^{then} parameters q_1, \dots, q_n are a set of generalized coordinates for the system if each \vec{r}_α can be expressed as a function of q_1, \dots, q_n and possibly by time t

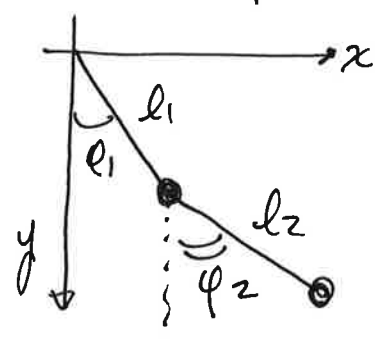
$$\vec{r}_\alpha = \vec{r}_\alpha(q_1, \dots, q_n, t) \quad \alpha = 1 \dots N$$

and conversely each q_i can be expressed in terms of \vec{r}_α, t

$$q_i = q_i(\vec{r}_1, \vec{r}_2, \dots, \vec{r}_N, t) \quad i = 1, \dots, n$$

- want smallest num gen coord n possible to parameterize system
 N free particles $\Rightarrow n = 3N$; constraints reduce this
 (e.g. rigid body $\sim 10^{23}$ atoms but 6 coord enough -
 COM posn; body orientation)

e.g. double pendulum. Single pendulum had 2 coord in principle, but only 1 needed as coord since length is fixed



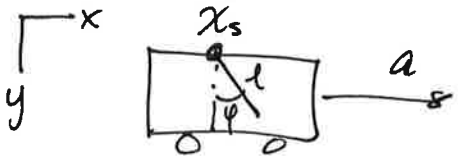
now: 2 bobs in a plane \Rightarrow 4 Cartesian coord

but! $\vec{r}_1 = (l_1 \sin \phi_1, l_1 \cos \phi_1) = \vec{r}_1(\phi_1)$

$$\vec{r}_2 = (l_1 \sin \phi_1 + l_2 \sin \phi_2, l_1 \cos \phi_1 + l_2 \cos \phi_2) = \vec{r}_2(\phi_1, \phi_2)$$

only need 2 generalized coordinates ϕ_1, ϕ_2 because l_1, l_2 constrained

Can depend on time. pendulum in accelerating car, \vec{a} given



bob support: $x_s = \frac{1}{2}at^2$

$$\vec{r} = (x, y) = (l \sin \varphi + \underbrace{\frac{1}{2}at^2}_{x_{\text{bob}} + x_{\text{car}}}, l \cos \varphi) = \vec{r}(\varphi, t)$$

issue here is inertial frame - if we analyze within car, non-inertial frame. We'd need a fictitious force to mimic \vec{a} , and Lagrangian won't work. Analyze from POV on ground.

- g_i are natural if they relate to Cartesian \vec{r}_x w/o time dep
- system is holonomic if it has n degrees of freedom and requires n generalized coordinates
 - requiring more? more complicated, we avoid!
 - example - rolling ball w/ mark on top
need 3 pos + 3 orientation coords
EVEN though only 3 degrees of freedom

7.4 more general: solid procs - review on your own

- action is stationary on right path even if there is a constraining force (e.g. normal force) to stay on a surface
- Lagrange eqns work for any holonomic system
 n deg freedom, n coord, non-constraint forces derivable from $\mathcal{V}(\vec{z}; t)$

how to find the force? $\mathcal{L} = T - U$. Let $U = U(g)$ indep t, \dot{g}

$$\frac{d}{dt} \frac{\partial \mathcal{L}}{\partial \dot{g}} - \frac{\partial \mathcal{L}}{\partial g} = \frac{d}{dt} \frac{\partial T}{\partial \dot{g}} - \frac{\partial T}{\partial g} - \frac{\partial U}{\partial g} = 0 \quad \text{but } F_g = -\frac{\partial U}{\partial g}$$

$$\Rightarrow F_g = \frac{d}{dt} \left(\frac{\partial T}{\partial \dot{g}} \right) - \frac{\partial T}{\partial g} = m\ddot{g} \quad \left. \begin{array}{l} \text{if } U \text{ indep } \dot{g}, \text{ as any consv.} \\ \text{force is} \end{array} \right\}$$

Examples

[SHO]

$$T = \frac{1}{2} m \dot{x}^2 \quad U = \frac{1}{2} k x^2 \quad \Rightarrow \mathcal{L} = \frac{1}{2} m \dot{x}^2 - \frac{1}{2} k x^2$$

$$\frac{\partial \mathcal{L}}{\partial x} = -kx = F_x \quad \frac{\partial \mathcal{L}}{\partial \dot{x}} = m\dot{x} \quad \frac{d}{dt} \frac{\partial \mathcal{L}}{\partial \dot{x}} = m\ddot{x} \Rightarrow m\ddot{x} = -kx \quad \checkmark$$

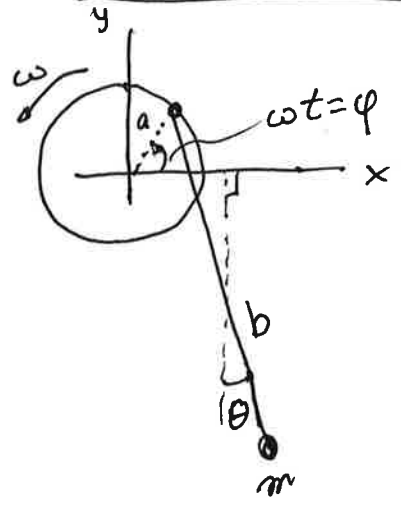
[gravity]

$$\mathcal{L} = \frac{1}{2} m \dot{y}^2 - mgy$$

$$\frac{\partial \mathcal{L}}{\partial y} = -mg = F_y \quad \frac{d}{dt} \left(\frac{\partial \mathcal{L}}{\partial \dot{y}} \right) = \frac{d}{dt} (m\dot{y}) = m\ddot{y} \Rightarrow \ddot{y} = -g \quad \checkmark$$

Pendulum on a wheel rotating w/ ω

(7.29)



just find coordinates of bob just

$$\left. \begin{array}{l} x = a \cos \omega t + b \sin \theta = x(\theta, t) \\ y = a \sin \omega t - b \cos \theta = y(\theta, t) \end{array} \right\} \begin{array}{l} \text{our} \\ \text{gen. coord} \end{array}$$

need \dot{x}, \dot{y} for T

$$\dot{x} = -a\omega \sin \omega t + b\dot{\theta} \cos \theta$$

$$\dot{y} = a\omega \cos \omega t + b\dot{\theta} \sin \theta \quad \text{chain rule...}$$

$$T = \frac{1}{2} m (\dot{x}^2 + \dot{y}^2)$$

$$U = mgy \quad \text{so } U(0) = 0$$

arbitrary shift would be irrelevant since only derivatives matter

$$\mathcal{L} = T - U = \frac{1}{2}m \left(\underbrace{a^2 \omega^2 \sin^2 \omega t + b^2 \dot{\theta}^2 \cos^2 \theta}_{\text{circled}} - 2ab\omega \dot{\theta} \sin \omega t \cos \theta \right. \\ \left. + a^2 \omega^2 \cos^2 \omega t + b^2 \dot{\theta}^2 \sin^2 \theta + 2ab\omega \dot{\theta} \cos \omega t \sin \theta \right) \sin(a-b) \\ - mg (a \sin \omega t - b \cos \theta)$$

$$\mathcal{L} = \frac{1}{2}m \left[a^2 \omega^2 + b^2 \dot{\theta}^2 + 2ab\dot{\theta}\omega \sin(\theta - \omega t) - mg(a \sin \omega t - b \cos \theta) \right]$$

clearly θ is our coordinate

$$\frac{d}{dt} \frac{\partial \mathcal{L}}{\partial \dot{\theta}} = mb^2 \ddot{\theta} + mab\omega (\dot{\theta} - \omega) \cos(\theta - \omega t)$$

$$\frac{\partial \mathcal{L}}{\partial \theta} = mb\dot{\theta}a\omega \cos(\theta - \omega t) - mg b \sin(\theta)$$

mb in every term

$$b \ddot{\theta} + a\omega (\dot{\theta} - \omega) \cos(\theta - \omega t) = a\omega \dot{\theta} \cos(\theta - \omega t) - g \sin \theta$$

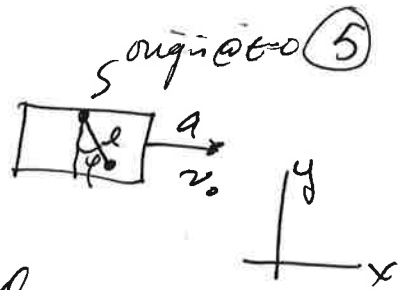
$$b \ddot{\theta} = a\omega^2 \cos(\theta - \omega t) - g \sin \theta$$

$$\ddot{\theta} = \frac{\omega^2 a}{b} \cos(\theta - \omega t) - \frac{g}{b} \sin \theta \quad \text{in principle done - can solve numerically}$$

let $\omega \rightarrow 0$? $\ddot{\theta} = -\frac{g}{b} \sin \theta$ usual pendulum
 simple view: period depends on angle non-simply
 imagine doing this with forces! turns out to be chaotic

* Wolfram demo *

Pendulum in an accel. car (7:30) from before



had $x = \underbrace{v_0 t + \frac{1}{2} a t^2}_{\text{car}} + \underbrace{l \sin \varphi}_{\text{bob rel car}}$

$y = -l \cos \varphi$
Choose y up now

$$\Rightarrow \dot{x} = v_0 + at + l \dot{\varphi} \cos \varphi \quad \dot{y} = -l \dot{\varphi} \sin \varphi$$

$T = \frac{1}{2} m (\dot{x}^2 + \dot{y}^2) \quad U = -mgl \cos \varphi$ only φ requ. as gen coord

$$\mathcal{L} = \frac{1}{2} m (v_0 + at + l \dot{\varphi} \cos \varphi)^2 + \frac{1}{2} m (l \dot{\varphi} \sin \varphi)^2 + mgl \cos \varphi$$

• can drop v_0 - will not survive derivations anyway
let $v_0 = 0$, still inertial frame

$$\begin{aligned} \mathcal{L} &= \frac{1}{2} m (a^2 t^2 + 2at l \dot{\varphi} \cos \varphi + \underbrace{l^2 \dot{\varphi}^2 \cos^2 \varphi + l^2 \dot{\varphi}^2 \sin^2 \varphi}_{l^2 \dot{\varphi}^2}) + mgl \cos \varphi \\ &= \frac{1}{2} m (a^2 t^2 + 2at l \dot{\varphi} \cos \varphi + l^2 \dot{\varphi}^2) + mgl \cos \varphi \end{aligned}$$

$$\frac{\partial \mathcal{L}}{\partial \varphi} = -mat l \dot{\varphi} \sin \varphi - mgl \sin \varphi$$

$$\frac{d}{dt} \frac{\partial \mathcal{L}}{\partial \dot{\varphi}} = \frac{d}{dt} (mat l \cos \varphi + m l^2 \dot{\varphi}) = mal \cos \varphi - mat l \dot{\varphi} \sin \varphi + m l^2 \ddot{\varphi}$$

$$m l^2 \ddot{\varphi} + mal \cos \varphi - mat l \dot{\varphi} \sin \varphi = -mgl \sin \varphi - mat l \dot{\varphi} \sin \varphi$$

$$l^2 \ddot{\varphi} + a l \cos \varphi = -g l \sin \varphi$$

$$\ddot{\varphi} = -\frac{a}{l} \cos \varphi - \frac{g}{l} \sin \varphi \quad (a=0: \text{regular pendulum})$$

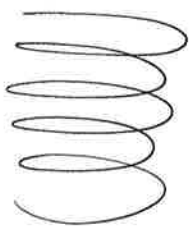
equ? $\ddot{\varphi} = 0$, or $g \sin \varphi = -a \cos \varphi \Rightarrow \tan \varphi_{eq} = -\frac{a}{g}$



physically - as it must be

can also show $\ddot{\varphi} = -\frac{\sqrt{a^2 + g^2}}{l} \sin(\varphi + \varphi_{eq}) \dots$ Small osc freq

Particle on a helical wire (7-20)



$\rho = R$
 $z = \lambda \varphi$

$v_z = \dot{z}$ $v_\varphi = R\dot{\varphi} \Rightarrow v^2 = \dot{z}^2 + R^2\dot{\varphi}^2$

$T = \frac{1}{2} m (\dot{z}^2 + R^2\dot{\varphi}^2) = \frac{1}{2} m \dot{z}^2 (1 + \frac{R^2}{\lambda^2}) = T(\dot{z})$

but $\dot{\varphi} = \frac{1}{\lambda} \dot{z}$... constraint of path eliminates two coord (b/c const R gets of me) - 1D problem!

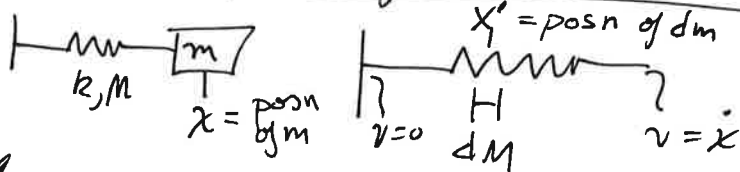
$U = mgz \Rightarrow \mathcal{L} = \frac{1}{2} m \dot{z}^2 (1 + \frac{R^2}{\lambda^2}) - mgz = \mathcal{L}(z, \dot{z})$

$\frac{\partial \mathcal{L}}{\partial z} = -mg$ $\frac{d}{dt} \frac{\partial \mathcal{L}}{\partial \dot{z}} = \frac{d}{dt} (m \dot{z} (1 + \frac{R^2}{\lambda^2})) = m \ddot{z} (1 + \frac{R^2}{\lambda^2})$

$\Rightarrow \ddot{z} = \frac{-g}{1 + R^2/\lambda^2}$

$R \rightarrow 0, a = -g$ - just falling!
otherwise, falls slower than free particle, depends on radius relative to pitch of helix

Spring w/ non-negl mass



assume v varies linearly for spring

$dT_s = \frac{1}{2} v_{dm}^2 dm$ $v_{dm} = \left(\frac{x'}{l+x}\right) v$

$dM = \left(\frac{M}{l+x}\right) dx'$
 $(l+x) =$ current length
 $x' =$ posn along spring

$T_s = \int_0^{l+x} \frac{1}{2} \frac{x'^2 v^2}{(l+x)^2} \frac{M}{(l+x)} dx' = \frac{1}{2} \frac{\dot{x}^2 M}{(l+x)^3} \int_0^{l+x} x'^2 dx = \frac{1}{2} \dot{x}^2 \frac{M}{(l+x)^3} \frac{x'^3}{3} \Big|_0^{l+x}$

$\Rightarrow T_s = \frac{1}{6} M \dot{x}^2$ as though $\frac{1}{3}$ of M moves w/ $\dot{x} = v_m$

$$\Rightarrow T = T_s + T_m = \frac{1}{2} m \dot{x}^2 + \frac{1}{6} M \dot{x}^2 \quad \mathcal{U} = \frac{1}{2} k x^2$$

$$\mathcal{L} = T - \mathcal{U}$$

$$\frac{\partial \mathcal{L}}{\partial x} = -kx = F_x \quad \frac{d}{dt} \frac{\partial \mathcal{L}}{\partial \dot{x}} = \frac{d}{dt} \left(m\dot{x} + \frac{1}{3} M\dot{x} \right) = \frac{1}{3} M \ddot{x} + m \ddot{x}$$

$$\Rightarrow kx + \ddot{x} \left(m + \frac{1}{3} M \right) = 0$$

$$\ddot{x} = \left(\frac{k}{m + M/3} \right) x \Rightarrow \text{SHM } \omega / \omega = \sqrt{\frac{k}{m + M/3}}$$

- effective mass includes $\frac{1}{3}$ of spring mass, lowers freq.
- is NOT damping though as you might have expected